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Use of a parametric finite-element model of the mitral valve to assess healthy and pathological valve behaviors

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1. Introduction

The mitral valve is the cardiac valve separating the left atrium from the left ventricle. It is composed of four elements: the anterior and posterior leaflets; the annulus which serves as insertion site in the heart muscle for the leaflets; the chordae tendineae which are attached to pillars in the ventricular wall and ensure that the very flexible leaflets remain within the ventricle; the papillary muscles which are located at the tip of the chordae tendineae and actively modify the tension acting on the leaflets. In the physiological case, the valve is open during diastole letting blood flow into the ventricle, and close during systole: the leaflets then create a hermetic seal between the two chambers preventing blood from regurgitating into the left atrium when ejected into the aorta. Mitral insufficiency is a valvular heart disease caused by a leaky mitral valve. It is the most frequent valvular pathology in Western countries after aortic narrowing upon calcification (Singh et al. 1999).

Mitral valve scan is the gold standard to obtain geometrical information. Anatomical studies have shown that human mitral valve measures may differ among patients (Gunnal, Farooqui & Wabale 2012, Khalighi et al. 2016), but generic patterns exist (Drach et al. 2015, Lau et al. 2010), which opens up the possibility to define parametric models of typical mitral valves. Several valve models have been developed in physiological conditions (Lau et al. 2010, Kunzelman, Einstein & Cochran 2007, Shen et al. 2017), but pathological conditions have been little studied. The aim of the present study is to develop a geometrical model of mitral valves in both healthy and pathological states.

2. Methods

2.1 Mitral valve definition

A mitral valve parametric model was created using FreeCAD software and Fortran subroutines, assuming a left-to-right symmetry and average geometrical parameter values (Table 1). It is constructed by defining points along the edges of the leaflets, which are then interpolated using b-splines.

The annulus of the mitral valve is defined using a planar D-shape, similarly to the Carpentier-Edwards Physio annuloplasty ring (Edwards Lifesciences). The papillary muscles tips are placed at fixed positions obtained from medical data (Sakai et al. 1999). The chordae tendineae are created as uniformly distributed chords going from the edges of the leaflets to the papillary muscle tips.

Anterior-posterior leaflet angles	8.3° - 5.3°
Leaflet height	7.7 to 23.4 mm
Leaflet thickness	0.8 mm
Annular width	4 cm
Annular height	3 cm

Table 1 Geometrical parameters used for the model.

2.1 Model of the mitral function

The closure of the mitral valve is simulated using a structure-only finite element method with the software ADINA v9.5. The impact of the blood flow dynamics on the valve deformation is indeed negligible when the valve is closed (Toma et al. 2016).

We solve for the displacement of the leaflets when subjected to a pressure profile composed of an initial linear ramp up to 0.1 s, followed by a constant plateau. The annulus and papillary muscle tips are fixed during the computation. The leaflet and chordae tendineae are assumed to be isotropic linear elastic, with Young modulus $E = 3$ MPa, Poisson ratio $\nu = 0.45$ and density $\rho = 10^3$ kg/m³. The contact is accounted for implicitly with a constraint function parameter set at 10^{-9} . We use a second-order implicit time integration scheme called Bathe scheme (Noh, Ham & Bathe 2013) and assume large displacements.

The leaflets are discretized using 4-node 3D-shells of maximum length 8×10^{-1} mm. The chordae tendineae are discretized using 2-node truss elements deforming in traction-only. The pathological case shown was obtained by rupturing some of the chordae tendineae attached to the anterior leaflet. It corresponds to a case where an asymmetry appears.

The linear part of the problem is solved directly using LU decomposition, and the non-linear part using the

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Newton-Raphson algorithm with a maximum of 15 iterations. A time step of 10^{-3} s is used from 0 s to 0.1 s and of 10^{-2} s hereafter. In addition, an adaptive time step method is used if convergence difficulties arise, the time step being then reduced to 10^{-7} s and 10^{-5} s, respectively.

3. Results and discussion

The stress distribution is plotted in the pathological (Figure 1) and healthy (Figure 2) cases. In the pathological case, a zone of higher stress than in the healthy case forms along the annulus. The valve is also not fully closed, which is a consequence of the lack of chordae tendineae attached to the anterior leaflet. The area of passage between the two leaflets can be quantified at systole to estimate valvular regurgitation. The anterior leaflet can be seen to protrude above the annulus plane in the pathological case, while it remains under it in the healthy case. The rupture of the chordae tendineae thus leads to the appearance of prolapse, which can be more easily detected thanks to imaging techniques than valve leakage itself, and can be of use to diagnose mitral regurgitation.

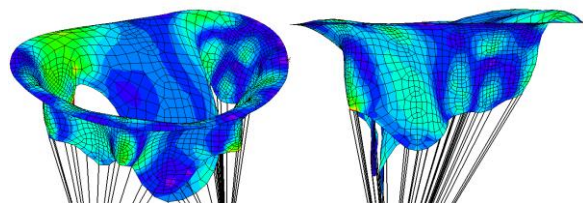


Figure 1 Stress distribution on the pathological valve at $t = 0.09$ s. Red is 1 MPa and blue is 0 MPa.

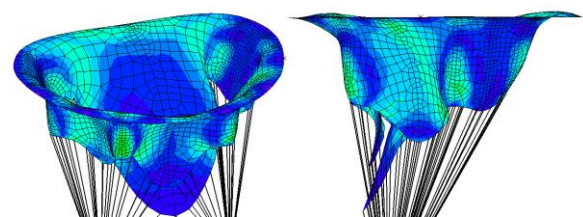


Figure 2 Stress distribution on the healthy valve at $t = 0.09$ s. Red is 1 MPa and blue is 0 MPa.

4. Conclusions

A geometrical model of the mitral valve capable of modeling healthy and pathological mitral valves has been built. The model allows to test several mitral valve geometries, and to assess in each case the mitral valve function using a finite element method. The model might be of use to numerically test medical procedures on mitral valves.

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